

VARIABLE SPEED DRIVES AND MOTORS

Installation Guidelines for Power Drive Systems



Developed by the joint GAMBICA/REMA Working Group

Installation Guide for Power Drive Systems

FOREWORD

This Technical Report has been produced to meet a demand for an authoritative guide on best practice for the installation of Power Drive Systems. It is the result of a study carried out by GAMBICA and REMA, taking note of well-established fundamental theory, technical papers, and carrying out specific investigations. The information given, while it can be applied to motors and inverters in general, is specific to current generation products of member companies.

The Technical Report principally considers the aspects of safe mechanical and electrical installation and the avoidance of EMC problems.

This report covers motors and inverters installed with a separate cabling system connecting the components together; it is not wholly applicable to inverters integrated into a motor design, which are now generally available up to 7.5 kW.

The references together with a useful list of further reading are included in the final section of this report.

SCOPE

This report provides information on the basic principles that require to be considered when specifying, and installing, a power drive system.

Supplies considered are low voltage up to 690 V a.c. The installation procedures detailed are specifically oriented to current United Kingdom practice.

For the application of a power drive system incorporating Ex. motors, refer to the motor manufacturer for confirmation of their suitability and certification.

SUMMARY

Satisfactory operation of a drive system is dependent on a satisfactory installation. Not only must the motor and converter be mounted in accordance with the manufacturers requirements, but they must also be adequately cooled, effectively cabled and earthed.

Compliance with the appropriate EU Directives, and with local regulations is also a legal requirement.

Specific sections in this report cover the requirements for the various parts of a power drive system, to assist specifiers and purchasers of drive systems from the specification phase to the installation and final commissioning.

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Section 1 INTRODUCTION

1.1 THE POWER DRIVE SYSTEM

A power drive system (PDS) is a concept used by a number of standards. It consists of a Complete Drive Module (CDM) and a motor, together with its interconnections; it does not include driven load. In turn the CDM consists of a Basic Drive Module (BDM) and its possible extensions such as the feeding section or some auxiliaries (for example ventilation). The BDM contains the electronic power converter, control and self-protection functions. Figure 1 shows the boundary between the PDS and the rest of the installation and/or manufacturing process.¹

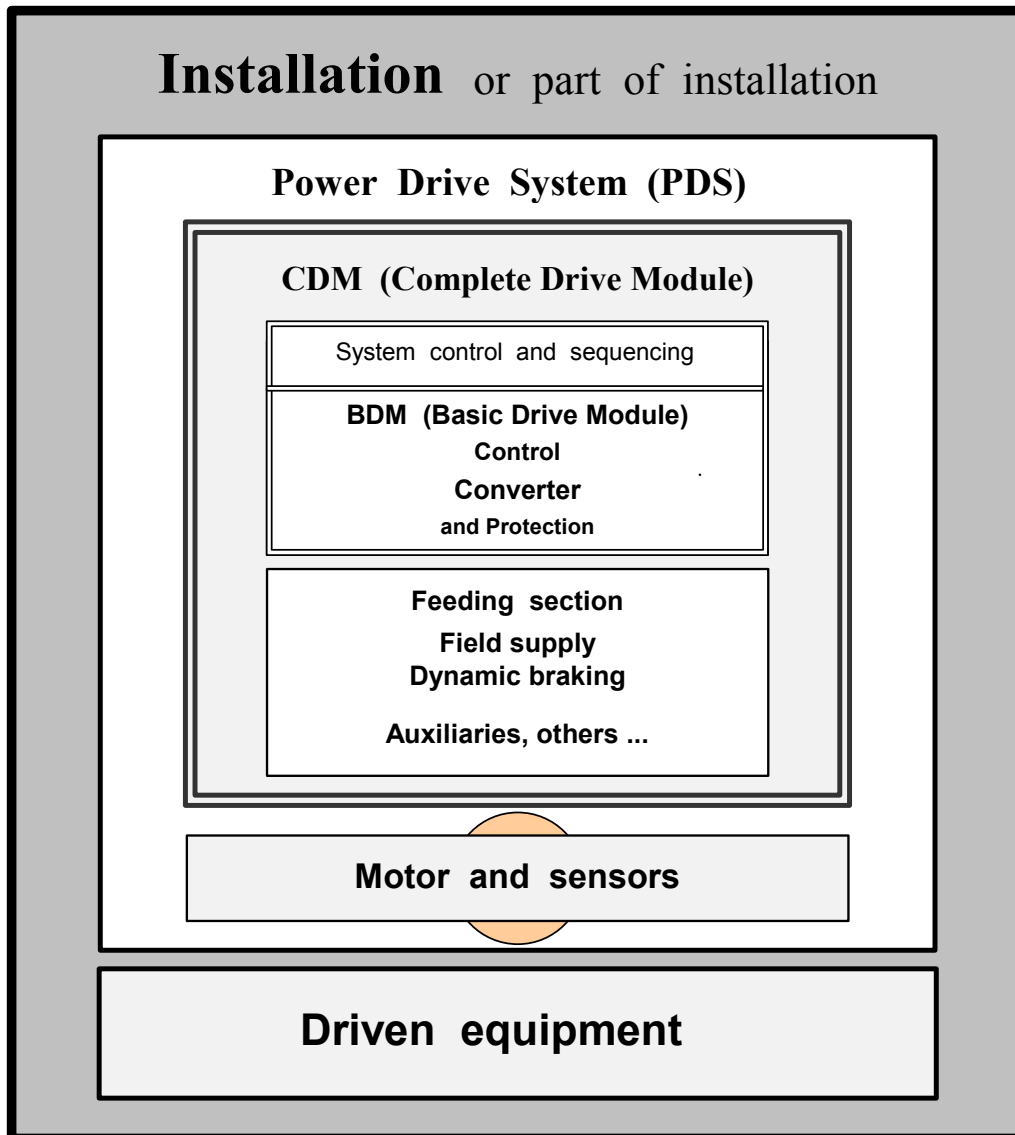


Figure 1 - The Power Drive System

¹ IEC 61800 part 1, 2 and 4 give details for these definitions.

For the purpose of this guide, the cabling from the supply is also considered, as the selection of suitable cables is often a problem especially when dedicated feeding transformers are installed.

1.2 THE MOTOR

The vast majority of motors sold today are squirrel cage induction motors; they are widely available, robust and efficient.

When installed in accordance with the simple guidelines given, they can be used in conjunction with a voltage source PWM drive to give a highly satisfactory variable speed drive system.

Specific requirements for motors are detailed in GAMBICA/REMA Technical Reports 1 and 2, which discuss winding insulation and bearing currents.

1.3 AC VARIABLE SPEED DRIVES

Variable speed a.c. drive systems as illustrated below are used in ever-increasing numbers because of their well-known benefits for energy efficiency and flexible control of processes and machinery using low-cost maintenance-free a.c. motors. Virtually all a.c. drives use power-switching techniques and generate high rates of change of voltage.

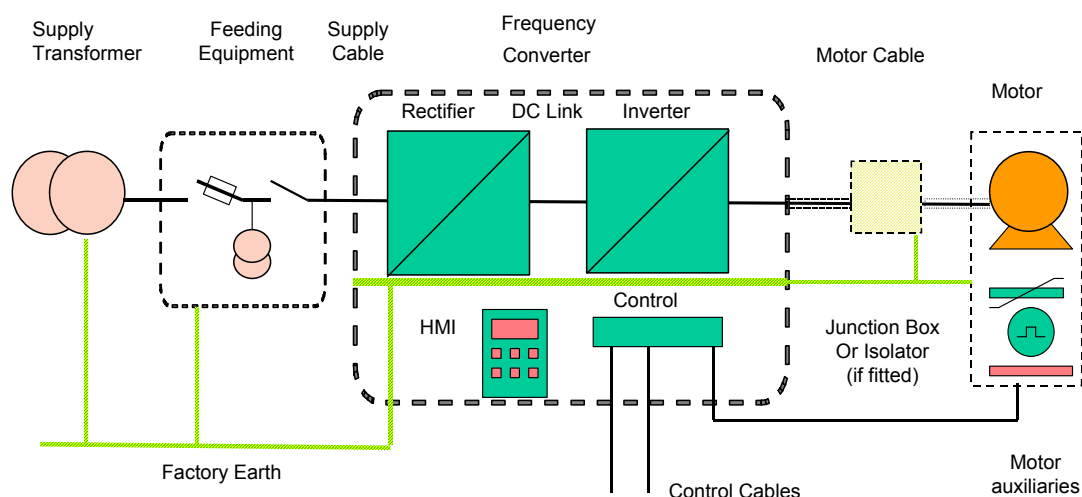


Figure 2 Power Drive System

Most modern a.c. drives incorporate a Basic Drive Module based on a voltage-source PWM inverter with very fast-switching power semiconductor devices such as Insulated Gate Bipolar Transistors (IGBT), which have the advantage of being very robust and having relatively low switching losses.

The nature of the voltage generated by such an inverter incorporates a certain degree of high frequency “noise”, which can lead to problems with Electromagnetic Compatibility (EMC). The rectifier also presents harmonic currents back to the network, which must be taken into account when designing a system.

1.4 THE TRANSFORMER

While most power drive systems are fed at low voltage from a supply shared with other equipment, there is occasionally a requirement to utilise a transformer in association with the drive.

1.5 THE CABLES

Cabling is one of the most critical areas of a good installation.

Section 2 THE MECHANICAL INSTALLATION

2.1 THE MACHINERY DIRECTIVE

Any installation in Europe must comply with the EU Machinery Safety Directive, which is designed to ensure safety for any user or operative.

EU Directives do not have the force of law in themselves - In the event of any problem in the UK, it is only the appropriate Statutory Instrument passed by the UK Parliament, which has force of law.

The Machinery Directive is known by the number 98/37/EC under which it was published in the Official Journal of the EU. The UK national legislation, which implements it, is The Supply of Machinery (Safety) Regulations 1992 (SI No 1992/3073) & Supply of Machinery (Safety) Amendment Regulations 1994 (SI No 1994/2063).

The Directive defines a machine as “an assembly of linked parts or components, at least one of which moves including the appropriate actuators, control and power circuits, joined together for a specific application, in particular for the processing, treatment, moving or packaging of a material”.

The Power Drive System is clearly, therefore, a part of a Machine.

To implement the Directive a number of standards are published – well over 400 are currently listed on the EU website.

CE Marking is the method used within the EU to indicate compliance with the appropriate directives for a particular item offered for sale; the presence of a CE Mark generally means that the equipment meets the relevant requirements. As the PDS is not a complete machine, it cannot carry a CE mark under the Machinery Directive. It should however, be delivered with appropriate declarations showing the standards that have been met.

2.2 SAFETY

A framework of standards regarding safety exists and the machinery manufacturer must identify the hazards associated with his specific equipment together with the corresponding safety requirements; he alone is in a position to do so.

The principle is to ensure that the risk associated with the system is acceptable.

The basic standards require that the PDS must be capable of being isolated whilst other hazards may require emergency stopping of the drive system, either by freewheeling to a stop on removal of power, or by active braking.

The location and type of any safety related requirements, such as emergency stopping, must be defined at the outset of the project.

In addition to these purely mechanical considerations for safety, the electrical safety of the system must also be considered (See Section 3)

2.3 ENVIRONMENT

The location of the parts of the power drive system must be considered, including -

- Altitude
- Ambient Temperature
- Humidity
- Possibility of condensation
- Ventilation
- Access
- Vibration
- Airborne contamination
- Noise
- Electrical Power Quality

2.3.1 MOTOR

Induction motors are very widely used around the world as prime movers in industrial, domestic and building environments. To acquire the greatest benefit from them, in terms of trouble-free operation and long life, it is very important that utmost attention is paid to all aspects of their installation. This becomes even more vital if motors are to be driven from an inverter supply, the nature of which could lead to unforeseen problems such as excessive vibrations, noise, bearing failures, insulation damage, mechanical damage, electrical or thermal overloading etc., if due care is not exercised.

There are many ways of mounting motors. They can be foot or flange mounted and mounting position can be horizontal or vertical with shaft up or down, or inclined at an intermediate angle. The mounting method and orientation must be specified to the motor manufacturer.

Normally, the motors are mounted on foundations, which must be solid, rigid and level. Slide rails, sunken bolts, and metallic base plates may be used to secure them to the foundations.

Direct-coupled motors can be mounted on bedplates or soleplates grouted in the foundations, or on pads or rods in special applications. When transmission is via belts, it is normal to use slide rails or an adjustable base, which permits the belt to be tensioned by moving the motor. Avoid the types of belt that are likely to become electro-statically charged.

Usually the location of the driven load will govern the location of the motor, and in general a wide range of motor enclosures are available to cope with the range of environments to be encountered. The correct level of ingress protection should be selected by reference to the appropriate standards.

Special attention should be paid to areas with particularly high (> 40⁰C) and low (<10⁰C) ambient temperatures, when special consideration may be required to ensure adequate cooling, lubrication, etc.

Attention should also be paid to installations where considerable levels of water spray are present, such as in cooling towers, to prevent ingress through the bearing seals.

In all these cases the motor manufacturer should be consulted to enable a suitable solution to be selected.

2.3.2 MOTOR INSTALLATION:

2.3.2.1 COUPLING

The transmission of power from the motor shaft to the driven equipment is achieved in a number of ways, broadly classed as solid and flexible.

Solid couplings lock the two shafts together allowing no relative motion between them; some axial adjustment is possible at assembly. They are used when accuracy and fidelity of torque transmission are of paramount importance, for instance, when the phase relationship between driver and driven equipment must be accurately maintained. Flexible couplings, depending on their individual design, can absorb a degree of axial, angular, parallel and torsional misalignment between the shafts. It is nevertheless important that during setting up of alignment, the manufacturer's instructions are strictly followed.

Whatever couplings are used, they should be aligned very carefully in all three planes. The shaft centres should be correctly aligned when in normal use so that they are coincident. The value of good alignment cannot be over-estimated. Poor alignment can be a major source of noise and vibrations. It may damage bearings, possibly shear a shaft and quickly ruin a flexible coupling. To ensure correct alignment, the manufacturers' instructions must be followed.

Allowance must always be made for shaft end-float and thermal expansion in both axial and radial directions.

Spline or gear-type couplings generally should be aligned to procedures similar to that of solid couplings. Coupling hubs should be heated in an oil-bath or oven prior to fitting; gas torches must never be used.



Figure 3 - Belt driven fan assembly

Belt drives have the motor mounted on slide rails or an adjustable base to permit re-tensioning of the belt by moving the machine. Whether it is flat-belt drive or V-belt drive, any limitation on pulley ratio and bearing radial loading must be strictly observed. Careful attention to the design of a belt drive in highly dynamic applications is always required.

2.3.2.2 BEARINGS

It is normal practice to pre-pack the bearings (ball/ball, roller/ball etc.) with grease before the motors are despatched from the works. In the case of non-shielded bearings, re-greasing facilities are provided as standard. Shielded bearings have sufficient grease to last over two years in normal operation.

If a motor has been stored for a long period, it may be necessary to re-grease the bearings with compatible grease before it is commissioned but care must be exercised to ensure that there is no over-filling of the bearing housings as this can cause over-heating of bearings. For practical purposes, the bearing housings of a normal non-vibrating assembly are considered to be full when the excess grease is rejected from them. The majority of the lithium-soap greases allow filling up to 90% of the free space in the housing. In special circumstances with vibrating assemblies, grease is packed to maximum of 60% of the bearing housing.

Re-lubrication intervals are load and temperature dependent and they are available on request from motor manufacturers. When replenishing, it is important that a right type of lubricant is used. Preferably, it should be the same as the one given on the motor nameplate. Using incompatible lubricants could lead to premature failure of bearings.

When motors are inverter-fed, the bearings may be subjected to damaging electrical discharges due to high frequency common-mode voltages. It is therefore important that correct precautions are taken.²

2.3.2.3 MAXIMUM EXTERNAL LOADS

A full list of values for both radial and axial forces can normally be found in motor manufacturers' catalogues. For a long and trouble-free bearing life, it is important that these values are abided by at the time of installation.

2.3.3 CONVERTER

Frequency converters use power electronic devices, which are relatively robust. However, the control electronics are generally assembled onto printed circuit cards with very close component spacing. They are therefore potentially vulnerable to contamination.

Specifically, condensation can have a disastrous effect, by allowing tracking across the surfaces of main semiconductors and of control cards, so it is of prime importance to prevent condensation within the converter enclosure, especially while the equipment is switched off. This also includes the effects of frost when a converter is installed in an unheated switch room during the winter. Means must always be installed to ensure that condensation is cleared away before energising.

² GAMBICA/REMA Technical Report No 2 gives recommendations.

Other sources of potential problems are corrosive gaseous contaminants such as hydrogen sulphide, which can even attack the alloys used for heat sinks.

The majority of commercially available drives are designed to operate when rigidly mounted, and are not designed to withstand high and repeated levels of vibration. Where high levels of mechanical vibration are likely to be encountered, the use of vibration damping mounts should be considered.

2.3.4 TRANSFORMERS

Some higher power drives use 12 (or more) pulse rectifiers to reduce harmonic distortion; this requires a power transformer to feed the phase-shifted inputs to the rectifiers.

There are two basic types of transformer - liquid cooled and dry type. All transformers have losses, both standing and load related, and must be installed in a situation where adequate cooling is available.

Contrary to the practice used for drives and motors the transformer rating is specified in IEC standards on the basis of a maximum +40 °C being reached occasionally, a monthly average of +30 °C and a yearly average of +20 °C. They are not designed for continuous operation at sustained high ambient. If this is required, then a de-rating must be applied.

2.3.4.1 LIQUID COOLED TRANSFORMERS

Liquid cooled transformers are generally designed for use outdoors. It is also usual to provide containment to ensure that any coolant leakage is restricted. The most common coolant is a mineral insulating oil, which is closely related to diesel oil. It is a potential carcinogen and is also flammable.

Other coolants include less flammable materials such as silicone oils, midel, and others. The manufacturers' recommendations regarding the nature of the hazards for these products must be followed.

It follows therefore that a COSHH³ review should be implemented before installing this equipment.

2.3.4.2 DRY TYPE TRANSFORMERS

Dry type transformers are of two basic types. Low voltage windings are usually resin impregnated in the same manner as motor windings, but many high voltage windings are resin encapsulated either in an autoclave or by wrapping techniques.

Dry type transformers may be installed in hostile environments and a number of classes exist. Typically a cast coil transformer will meet Class C2, which requires a thermal shock to be applied, Class E2, which requires the equipment to operate satisfactorily in high humidity, and F1, which determines the fire retardant capability.⁴

2.4 CABLES

It is important to plan the cable installation carefully. The installation may require bottom cable entry for the cables running in trenches, or top entry from cables on tray

³ Control of Substances Hazardous to Health.

⁴ IEC 60726

work. It is important with either arrangement to ensure the segregation detailed later is maintained.

It is also of primary importance to ensure that the equipment is suited to cable entry from the direction required, and to ensure that water and foreign matter cannot enter through the cable entry or cable gland plate.

Many armoured power cables are extremely intractable and difficult to bend; therefore allowing adequate bending radii is always important. In drive installations the armouring also forms an essential part of the electrical screening and the minimum bending radii detailed by the manufacturer must always be observed to prevent the wire armour spreading thus leaving slots to radiate HF emissions.

2.5 EQUIPMENT SITING

2.5.1 MOTOR

Motor siting has been discussed in 2.3.1. However, the availability of free access to the cable boxes for installation and maintenance must be considered as should the access to bearing greasing points when provided (generally in motors >75 kW).

It is advisable to install the motor with adequate access for routine maintenance. A minimum clearance at the fan inlet is necessary to ensure free airflow, this can vary from 50 mm for low power (<11 kW) to 150 mm or more for a high power motor. Ensure that there is no obstruction to the cooling airflow and that the inlet and outlet apertures are clear.

Any motors that are mounted vertically must be protected from falling objects entering the fan housing.

2.5.2 CONVERTER

With the exception of some motor mounted converters (sometimes referred to as integral motors) the converter is designed for indoor installation. The preferred solution is always to mount drives in custom plant or control rooms, both for safety, by restricting access, and to ensure an optimum operational regime.

Drive losses have to be dissipated. This is generally to the ambient air in the control room; therefore the largest possible room volume is helpful.

The majority of converters are fitted with cooling fans to circulate cooling air across the heat sinks. Any restriction to this air path reduces the efficiency of the cooling system.

Smaller power drives associated with specific items of plant or machines installed indoors may be mounted locally to the machine provided that adequate protection is possible.

Enclosure ingress protection should be selected as the minimum level commensurate with safety. Filtering cooling air involves maintenance and in time the filter mats are often discarded, leaving the drive unprotected.

Where drives are mounted on a wall, this should preferably be of brick or block construction.

Larger power drives can have their discharge ducted to outside air, where extreme care must be taken to avoid condensation forming in the ductwork. Consideration

may also be given to water-cooling. This may be by utilising a proprietary water-cooled drive system, or by installing water/air coolers in the control room.

Where the air flow through the main heat sinks is ducted outside the control room, or where water cooling is used, there will still be some heat dissipation into the control room e.g. due to cabling and the control electronics. The drive manufacturer will advise on the magnitude of this dissipation.

2.5.3 COOLING REQUIREMENTS

The majority of drives are designed for a maximum ambient temperature of 40°C, which means that the inlet cooling air must not exceed that value.

This in turn suggests that to maintain an acceptable room temperature a suitable level of airflow will be needed.

The basic formula to determine an airflow in cubic metres per hour is to multiply the heat loss in Watts x a constant (3.1 for air at sea-level) and divide by the temperature differential in K.

These requirements are equally valid for drives installed in secondary enclosures.

In the event of manufacturers' figures being unavailable, the loss can be assumed to be 2.5% of the controlled motor power for each inverter. If transformers are installed in the same room a similar allowance should be made for each transformer.

As a typical example – a standard 6 pulse a.c. drive rated at 75 kW with the converter mounted in a switch room with an ambient temperature of 30°C and an anticipated temperature differential of 10K will require $0.025 \times 75000 \times 3.1 / 10 = 581 \text{ m}^3/\text{h}$.

These values are in addition to those for dissipating losses from switch and control gear.

The maximum surface temperature of any parts that may be touched must also be considered.

In multi drive installations the diversity of loading should be considered, since this may offer savings in the cooling requirements.

The airflow must be arranged to ensure that no recirculation of the heated exhaust air occurs. It must also be remembered that warmed air expands; therefore if free ventilation is required the outlet should be at least 20% greater cross sectional area than the inlet. In addition to cooling the equipment adequately, the prevention of condensation is also critically important. For effective prevention a dry transformer, motor or converter enclosure should be kept at least 10K warmer than the surroundings. Generally heaters are sized according to the formula

$$H = \Delta t \times A \times k$$

Where H = Heater Power (Watts)

Δt = Temperature differential (K)

A = Surface area in m^2

k = constant (typically 5.5 W/Km^2 for painted sheet steel).

Details on the selection principles for secondary enclosures can be found in the GAMBICA Technical Guide – General Purpose Enclosures.

Section 3 THE ELECTRICAL INSTALLATION

3.1 THE LOW VOLTAGE DIRECTIVE

Any electrical equipment supplied in the European Union or European Economic Area, except those in a hazardous area, utilising voltages below 1000 V a.c. or 1500 V d.c. must comply with the EU Low Voltage Directive, which is designed to ensure electrical safety. The ATEX directive covers safety in hazardous areas. The Low Voltage Directive is implemented in a similar manner to the Machinery Directive as previously described.

3.2 BASIC REQUIREMENTS

The electrical installation of the equipment covers aspects such as

- Insulation
- Provision for isolation
- Cable selection
- Overload and fault protection
- Earthing

All of these aspects must be undertaken correctly to ensure a safe and satisfactory installation.

Any installation must be undertaken in accordance with the appropriate National Regulations. Requirements that are specific to a power drive system are considered in detail in the following sections.

3.2.1 GENERAL REQUIREMENTS

With regard to the electrical installation, the equipment suppliers' instructions must be observed. Before any electrical connections are made, check there is no foreign matter present and if there is any surface dust or dirt, ensure it is removed.

3.2.1.1 MOTOR

To make electrical connections, a connection diagram, which is normally provided in the terminal box of the motor, must be carefully followed. The connecting links must be correctly set for the appropriate voltage. Cabling practice is described in the following paragraphs. If a motor is fitted with a feedback device, such as a digital tachometer (commonly referred to as an encoder) or a resolver, ensure pin connections are correctly made.

The terminal connections must be made with utmost care, ensuring that there is sufficient clearance and creepage distances between the adjacent terminals. The cable end lugs must be properly secured to the studs of the anti-tracking terminal block using washers and nuts provided but excessive torque to the terminals must be avoided as this can result in damage to them.

When auxiliary devices, such as Resistance Temperature Detectors (RTDs), thermistors or thermostats, are located in the stator winding, they must be connected to a suitable control circuit in the inverter cabinet to give an alarm, or trip the drive at a predetermined temperature.

Where anti-condensation heaters are fitted on to the stator windings, they must be connected to a suitable supply and control must be arranged such that they are disconnected whilst the motor is energised. They should only be energised when the motor is de-energised. The operation of any auxiliary device should be checked.

Motors on their own, when operated direct from the public electricity supply network, are benign in respect of electro-magnetic interference, both in terms of immunity and emissions. When used in conjunction with inverters, they become part of the power drive system and therefore, can no longer be considered benign. More information is provided in Sections 4 & 5.

Finally, recommendations for insulation and bearing requirements are given in GAMBICA/REMA Technical Reports 1 and 2.

3.2.1.2 CONVERTERS

It is of paramount importance that the manufacturers' instructions and diagrams with regard to wiring are adhered to. Connecting a mains supply to the converter motor terminals can cause serious damage to the installation.

3.3 THE TRANSFORMER

In general the electrical installation of a drive-dedicated transformer is no different to any other power transformer. The transformer cables should follow the guidelines given for drive input cables, unless the manufacturer makes a specific recommendation, for example where a 12 pulse rectifier is utilised.

The electrical protection of a transformer requires care, and must always be carefully considered. Protection is normally required for over current and over temperature as a minimum. It is usual for the over current protection to include the primary and secondary cables.

Dry type transformers will normally have resistance temperature detectors (RTDs) that must be monitored, and the primary disconnected in the event of a problem. Liquid cooled transformers have contact thermometers or RTDs plus monitoring for the coolant pressure and condition.

3.4 POWER CABLE TYPES

3.4.1 DRIVE SUPPLY CABLE

There are no special considerations for the selection of input cable types when using a PDS. The cable should be chosen to suit the installation.

3.4.1.1 FAULT CURRENT CONTRIBUTION AND CABLE SIZING

Unlike a motor directly connected to a network, a diode rectifier fed drive will not produce any contribution to a fault in the supply network. A regenerative drive will only feed a current equal to its rating, while the control is energised.

3.4.2 DRIVE MOTOR CABLE

Drive output cables should always be multicore types, and the use of single core cables is to be deprecated.

Where a single cable is inadequate for the current rating, parallel multicore cables should always be used.

The following additional issues must be considered:

3.4.2.1 CABLE CAPACITANCE

The drive has to provide charging current for the cable capacitance at every PWM pulse edge, and this forms an additional current load on the drive which can, if excessive, cause it to trip or invoke a premature current limit. The drive supplier should specify a maximum cable length, with an indication of the type of cable used.

It is usually possible to extend the limit by the use of output chokes, or filters at the drive terminals. The use of output devices will result in a voltage drop, which should be taken into account when selecting the motor.

Some types of cable have exceptionally high capacitance and in these cases reduced limits may apply. The drive supplier should be consulted. Some examples of cables with high capacitance are:

- Mineral insulated copper clad cable
- Screened cable where the screen is laid directly on the phase cores, with no intervening insulating jacket

The maximum cable length will vary with the drive rating and whether input or output filtering is installed, and will generally increase with increasing power. As a general guide, in the absence of special filtering considerations, if the cable length exceeds 50m then the drive supplier should be consulted.

3.4.2.2 CABLE SCREENING

It is strongly recommended that the cable be screened. This is essential in order to meet many of the relevant EMC standards, and is recommended in any case to reduce the risk of interference to other equipment. The screen will have to carry relatively high amplitude current pulses, therefore its RF impedance and connection method at each end are critical.

Effective forms of screen are:

- Copper braid
- Copper tape
- Close wound galvanised steel wire armour
- Aluminium tape armour
- Steel braid
- Solid copper cladding

To be effective, the screen must have good electrical continuity along the cable length. The braided or helical construction must be such that current can easily pass from turn to turn along the length. The screen coverage must be as close as possible to 100%, and the resistance must be low, especially at high frequencies.

The following are less suitable for their screening capabilities:-

- Galvanised steel spiral tape
- Screwed steel conduit
- Cables with thin foil screens
- Cables with open woven braids

3.4.2.3 PROTECTIVE CONDUCTOR (EARTH) CONNECTION.

To meet the EMC and availability requirements, only shielded, multicore cables should be used. Some exceptions to this rule are given in the product specific manuals.

To be effective at high frequency, the shield conductance shall be at least 1/10 of the phase conductor conductance. One way of evaluating the effectiveness of the shield is the shield inductance, which must be low and only slightly dependent on the frequency.

These requirements are easily met with a copper or aluminium shield/armour. The cross section of a steel shield has to be ample and the shield helix of low-gradient. Galvanizing will increase the high frequency conductivity.

The question of whether the cable screen can be used as the protective (earth) conductor depends on the safety regulations being applied, on its resistance relative to the phase conductors and on the prospective fault level.

To operate as a protective conductor, the shield conductance must be at least 50% of that of the phase conductor.

If a separate protective conductor is required, then it must comply with one of the following options:

- Be entirely outside the cable screen
- Be entirely inside the cable screen, and terminated by a very short connection at the same place as the screen at both ends of the cable.

Any other arrangement will reduce or remove the screening benefit of the cable.

3.4.2.4 SYMMETRY

Very large numbers of successful installations have been undertaken with 4 – core shielded cables, however, there is some evidence to suggest that for larger cables a symmetrical construction will give an improved performance, i.e. either there should be no internal protective conductor or else there should be three internal protective conductors symmetrically arranged with respect to the phase conductors.

The object of the symmetry is to achieve an even field within the cable screen, which will reduce the induced voltages on the protective conductor, and therefore limit any potential difference applied to a motor frame, which will induce shaft voltages and potentially cause motor bearing damage.

This effect becomes more apparent with increase in size and cable run, while the application of output filters can reduce this requirement.

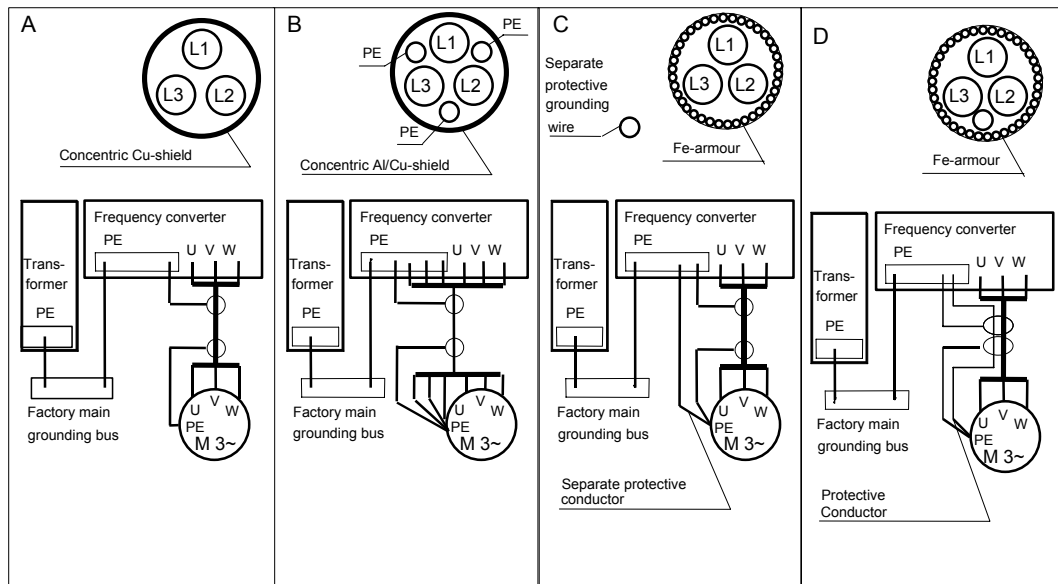


Figure 4 Typical Converter/Motor Cables

3.4.2.5 VOLTAGE RATING

Standard 600/1000V mains-rated cables are suitable for this application. It has sometimes been suggested that because of the repetitive voltage transients caused by pulse reflections in the cable, special cable with additional insulation should be used. This may be the case for large drives operating at voltages above 690V, but for applications at or below 690V there is no requirement for special insulation.

3.4.2.6 INCLUSION OF OTHER CABLES

No other cables, neither power cables nor data/signal cables, should be included within the motor cable screen. Very high levels of electrical noise will be induced into such cables. Although it is possible to accommodate this by careful management, it is not recommended for general use.

3.5 CABLE RATINGS

The cable rating should primarily be based on the electrical safety and wiring regulations applicable in the end product or the intended place of use of the installation. This must take account of the ambient temperature and the mounting arrangement for the cable in so far as it affects the cooling capability.

In the UK cables are normally rated in accordance with BS 7671 (The IEE Wiring Regulations) and IEC 60287. However, the specific manufacturer's rating tables should be applied, as these take into account the specific cable construction.

The worst-case method of installation must also be taken into account. For example, where a cable is installed for the most part on a tray in air, it may also pass through a restricted transit. In this case, this transit must be considered as the installation method in order to avoid hot spots and thermal problems.

The following additional issues must be considered:

3.5.1 SUPPLY AND MOTOR CABLES

- Continuous r.m.s. input supply and motor output current ratings of the drive.

Note that the short-term overload rating of the drive is typically for too short a duration (e.g. 1-min) to affect the cable rating directly. However it may have an indirect effect by determining the rating of the protective device.

- Voltage drop

For long cable runs, it may be necessary to increase the cable rating beyond the requirement for safety in order to restrict the cable voltage drop. However the effect of voltage drop is much less severe with a VSD than with a direct-on-line started induction motor. The intelligent control of even the simplest drives limits the starting current in the motor circuit to (typically) 150% of the full load rating. This provides a starting torque that is not affected by voltage drop in the input cable and can be optimised to allow for the voltage drop in the output cable.

The cable voltage drop does affect the available torque at maximum speed, and especially for drives that operate beyond the motor base speed (field weakening). For applications where this is an important consideration this aspect must be given attention. Even then, many drives offer slip compensation that can maintain the torque at the expense of an increased motor current.

When standard design codes are used for cable selection they should be configured for resistive loads and not for motor loads, otherwise unnecessary cost may be incurred in allowing for the starting current.

3.6 SUPPLY CABLE

- Co-ordination with the protection device (fuse or circuit breaker).

This device provides protection to both the drive and the cable, so the cable must be selected appropriately. When using standard industrial fuses such as the BS-EN 60269 gG range, which are designed for co-ordinated protection of cables against faults and overloading, the cable rating must simply equal or exceed the fuse rating (allowing for ambient temperature).

- Effects of inrush current

A frequency converter will have an inrush current on charging that is LESS than its full load current, therefore no provision in cable sizing is needed to cover this aspect. If a transformer is installed, a substantial inrush of very short duration is to be anticipated.

- Effects of harmonic currents.

Most drive rectifiers generate harmonic currents back to the network, these tend to increase the overall r.m.s. current flowing between the drive and the supply. Line reactors in the a.c. or d.c.link chokes will provide some harmonic mitigation, and reduce the effective r.m.s. current.

Typically, the total r.m.s. current of a 3 phase 6-pulse drive at full load is very similar to the rated output current.

For single-phase input drives this assumption cannot be made, and the manufacturer's listed input current must be used for dimensioning.

- Skin effect

Another factor influencing the cable carrying capacity is "skin effect" which causes an increase in cable losses due to high frequency currents. These relative losses increase with increasing conductor size. Typically the cable de-rating factor for a 6-pulse rectifier due to skin effect will vary from negligible levels up to 35 mm², 1% with 50 mm², increasing to 4% with 300 mm². These figures may be very small but do indicate that cable sizing should not be skimped.

Some further guidance on cable de-rating for harmonics is given in IEEE519 and in IEC 60092-352, (Cables for Marine Installations) while there are currently no European standards for industrial applications.

3.7 MOTOR CABLE

- Co-ordination with the protection provision

The drive provides fast-acting short-circuit and earth-fault protection which protects the motor, cable and drive. Overload protection of the motor is also provided, usually within the drive but possibly by a separate device where multiple motors are connected to a single drive. Provided this protection has been correctly arranged the cable rating needs only to match the motor continuous rating.

- Effects of harmonic currents.

The inverter produces a series of voltage pulses in the output, this results in a virtually sinusoidal output current. There is therefore no need for any special consideration.

- Other factors

Other factors detailed for input cables also need to be taken into account when selecting motor cables.

3.8 CIRCUIT PROTECTION

Most drive modules require circuit protective devices (fuses or circuit breakers) at the supply input. Their purpose is to provide protection from a catastrophic failure within the drive, which causes a fault between lines or to earth, or (rarely) a sustained overload.

Protection against drive or motor overload and against a short-circuit at the output is provided in the drive.

The drive supplier's recommendations must be followed. This is essential for the safety of the installation, and to maintain the validity of safety markings such as the CE mark, UL approval etc.

Most small drives can be protected by standard industrial power fuses such as the IEC 60269 gG range, or by a corresponding MCB or MCCB. For some designs it may be necessary to use special fast-acting semiconductor fuses to prevent serious

damage to the drive following an internal fault. In this case it will generally not be possible to use a MCCB.

In all cases where MCBs or MCCBs are intended to be utilised the initial let through values should be checked, as some MCBs have a relatively slow initial action, while giving the desired let through characteristic.

Where high-speed fuses are used to protect the PDS, it is often possible to use lower RMS rating slow fuses to protect the cables feeding the PDS and, as in all installations, the overall discrimination needs careful assessment.

3.9 HIGH POWERS/CURRENTS

When high powers are involved, and it is not possible to obtain an adequately rated single three-core cable, or the physical installation of such a cable is too difficult, the installation should be made in parallel three core cables, not in single core cables. This is to prevent circulating currents in the screens of single core cables, as the screen must be terminated at both end.

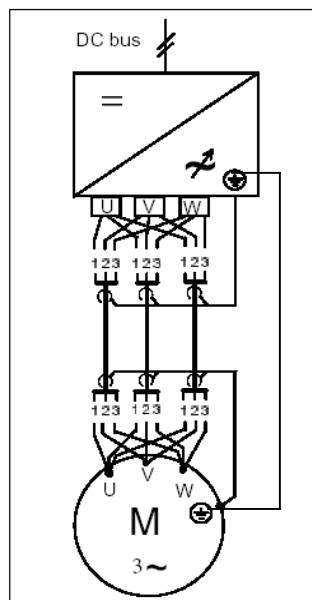


Figure 5 – High Current Installation

3.10 CABLE CONNECTION POINT

Even when a drive is mounted in a secondary enclosure, the cable connecting points on the drive module should preferably be used, and intermediate connections avoided.

3.11 LOCAL TO MOTOR ISOLATION

Where local to motor isolation is required for safety purposes, it is essential that the switch enclosure should be conductive, and form part of the “Faraday Cage” surrounding the entire PDS. This means that the cable screens should be correctly bonded/glanded to the enclosure.

In many cases the converter manufacturer will make recommendations regarding switching off the inverter, prior to opening of the switch contacts.

3.12 OUTPUT CIRCUIT SWITCHING

The majority of PWM drives use a conventional control, and it is generally possible to include a switch in the output of the inverter without causing damage. Some converters use more sophisticated predictive control – these include flux vector and Direct Torque Control (DTC) designs – where the drive has an integrated software motor model, and it is possible that opening the output circuit can cause the drive to attempt to force a higher voltage at its output to maintain the motor current. In these circumstances it becomes difficult for the switch to clear the arc, and the inverter switching should be inhibited before allowing the contacts to open. It is always good practice to inhibit the inverter before output switching.

3.13 CABLE GLANDING

Whenever screened cables are used, it is essential that they are “properly” glanded and terminated, that the screen/armour makes contact through 360° to the gland and also that the gland is circumferentially grounded to the gland plate and to the main earth terminations.

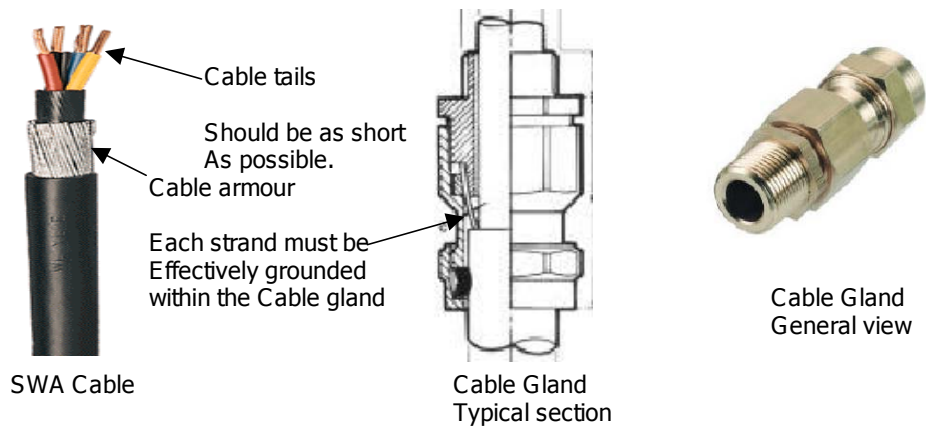


Figure 6 - Typical Cable and Gland

3.14 POWER FACTOR CORRECTION

With a frequency converter no power factor correction capacitors should be installed in the motor circuit. The inverter provides the reactive power.

Voltage source PWM type frequency converters have an inherently high power factor due to the uncontrolled or active rectifier design, and in general do not require power factor correction.

Where power factor correction is required for other equipment connected to the same bus, care must be taken to avoid harmonics from the drives damaging the capacitors, and de-tuning reactors should generally be used.

In addition group power factor correction batteries can lead to high switching transient voltages, which must be limited by restricting the maximum reactive power switched in one stage to:

$$Q_m = \frac{S_n}{2.5 \times Z_k}$$

where

Q_m = Maximum permissible capacitor reactive power (kVAr)

S_n = Rated power of supply transformer (kVA)

Z_k = Short circuit impedance of supply transformer (%)

3.15 CONTROL CONNECTIONS

The control interfaces to a PDS are at least as important as the power connections.

3.15.1 ANALOGUE SIGNALS

Analogue and very low voltage digital I/O signals should always be made in twisted pairs, with the twist carried as close as possible to the appropriate terminals. If possible, avoid the use of a common return for different analogue signals.

Double-shielded cables will give the best performance.



Figure 7 Double screened twisted pairs

Unless otherwise stated in the installation instructions for the particular equipment, the cable screen should be bonded at both ends.

The cable screen should be bonded at the screen termination points provided by the equipment manufacturer. These should not be confused with the “0 Volt” or “Signal Ground” terminals that may also be provided.

Cables should be connected as in the following diagram:

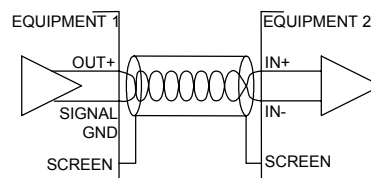


Figure 8 Control cable connection

An example of bad practice is shown in the following diagram:

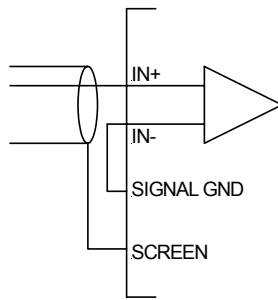


Figure 9 Incorrect control cable connection

Here, the negative input has been connected to a local 0 Volt connection, instead of the negative output of the signal source. This results in the input being susceptible to common-mode noise. If the signal source is single-ended, the IN- input should be connected to the 0 V reference of the signal source.

3.15.2 DIGITAL SIGNALS

Always separate digital and analogue signals. Never mix 110/230 V digital signals in the same cable as 24 V DC signals. A conventional screened or armoured cable can be used for 110/230 V signals.

3.15.3 SERIAL COMMUNICATION SIGNALS

The appropriate cable will depend on the carrier medium, be it RS 232, RS 485, Ethernet, etc. Follow the system recommendations.

3.15.4 ENCODER CABLES

Pulse encoders may be galvanically connected to the motor rotor; it is important that any bearing insulation is not bridged. The recommendations of the encoder and drive supplier should always be strictly followed. The correct cable type is also essential.

It is also preferable to ensure that the cable run from the encoder is a continuous length and not interrupted by screw terminals.

3.15.5 SEGREGATION

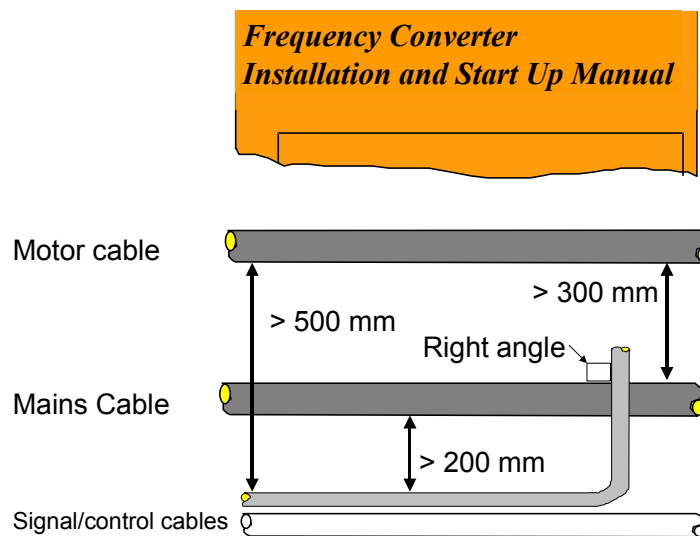


Figure 10 Recommended Segregation between cables

Many installers are reluctant to bond a cable screen at both ends due to a fear of circulating currents. Drive manufacturers are well aware of this, but have tested their products to meet the most stringent operating conditions. They include instructions for appropriate mitigation measures, such as potential equalisation conductors in parallel with the screened cables.

The screen termination may only be omitted at one end if the signal at that end is galvanically isolated, and the manufacturer of the equipment specifically approves of this style of connection.

Section 4 EARTHING

Primarily the purpose of earthing is personnel safety. Irrespective of any other instructions all the conducting parts of the PDS frames must be earthed, ensuring that a safe “touch voltage” is not exceeded. The requirements of BS 7671(The IEE Wiring Regulations) must always take precedence.

For electromagnetic compatibility it is also necessary to ensure that equipotential bonding is effective over a wide range of frequencies.⁶ Further information on Earth Bonding and Electronics is also contained in EN 60204-1.

In order to limit the potential for a system to radiate noise, it is essential that all the parts share a common potential. Because of the high frequencies involved, this means that the conductors connecting them must have very low inductances. For this reason the conductors required from the safety point of view are often inadequate. Sizing of earth and PE conductors is discussed in the EMC issues.

It is also important that both the motor and driven machine share a common earth potential, and the drive and its controls share a common potential.

4.1 SUPPLY CONNECTIONS

4.1.1 EARTHED SECONDARY (TN, TN-C, TN-S)

In these network connections the neutral is earthed at the point of supply; normal drives with EMC filters can be used. A TN-C network uses a common earth and neutral conductor, which is not recommended; a TN-S system should always be utilised to ensure a single earth-neutral bond.

4.1.2 UNEARTHED SECONDARY (IT)

These networks are commonly found in hospitals, in certain crude oil pumping installations and in the secondary connections of 12 pulse drives. An isolation transformer or other separately derived source normally supplies the unearthed system. A particular feature of this system is the absence of a direct connection between the phase and neutral (if present) conductors and earth. As a result, the fault current is relatively low in the event of an insulation fault. In fact, its magnitude is primarily limited by the system leakage capacitance. As might be expected, the upstream protective device will not trip due to a first fault.

It is possible for the equipment to continue to function in the event of a single earth fault. Earth leakage monitoring is a mandatory requirement to alarm in the event of a first earth fault and allow safe disconnection before a second earth fault.

EN 61800-3 recommends that EMC filters should not be used in un-earthed networks.

⁶ GAMBICA/REMA Technical Report No 2 covering Bearing Currents gives further information on the requirement for potential equalising.

High levels of common-mode voltage can occur in IT systems such as those used with 12 pulse drives, which will share the electrical stresses on the motor windings with the input circuit and transformer. This is not a potential problem with I.v. networks; however, the manufacturers' recommendations for cable insulation levels for higher voltage systems should be sought.

4.2 EARTH FAULT PROTECTION

4.2.1 SUMMATION PROTECTION

A current summing (core balance) transformer is normally used to detect an earth fault current in an earthed network. In case of an earth fault, the current imbalance produces an earth fault warning or trip, depending on the requirements.

4.2.2 INSULATION MONITORING

The high reliability of an IT system (including an isolated 12 pulse system) is assured by continuously monitoring the insulation level of the system. The insulation-monitoring device detects insulation faults at an early stage as they are developing and provides a signal that can be used to trigger visual and audible alarms when the insulation level drops below its set point. The insulation resistance can generally be monitored over a period.

4.2.3 EARTH LEAKAGE PROTECTION

Earth leakage protection using a Residual Current Device (RCD) or similar is predominately used for the protection of personnel and requires special attention with an a.c. VSD, for the following reasons:

- i. The drive contains a rectifier, which could cause a smooth d.c. earth current. For this reason only a type B RCD can be used with a VSD.

Note A type A RCD must **never** be used up-stream of an a.c. VSD. It could become disabled by the presence of smooth d.c. residual current and fail to provide protection for other loads.

- ii. The majority of drives have a significant residual current, both at the supply frequency, because of the presence of RFI filter capacitors between lines and earth, and at frequencies related to the PWM, because of the effect of the capacitance from the motor circuit to earth. This can cause nuisance tripping of the RCD.
- iii. Further details on the selection of RCDs for a drive are given in IEC 61800-5-1 Annex E.

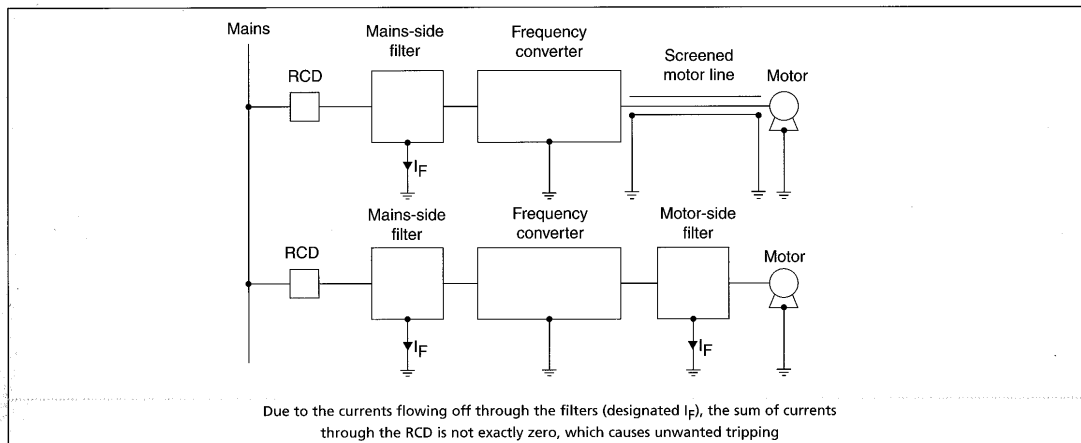


Figure 11 Interference paths for RCD operation

The likelihood of such problems depends to some extent on the frequency response of the particular RCD, which is not necessarily a parameter that is specified or controlled by the manufacturer although some manufacturers will offer units specifically designed for use with VSDs.

In cases where the RCD can be set at over 300mA, problems are less likely with lower power drives unless very long motor cables are being used, or considerable numbers of drives are connected to the same RCD.

If RCDs are specifically required, some drive suppliers offer low-leakage RFI filters as an option. This generally only works with short motor cables; alternatively it may be necessary to use an isolation transformer at the drive input.

It should also be noted that an a.c. VSD also incorporates large capacitors in the d.c. link, which store charge, also if a high inertia load is connected substantial kinetic energy may be available to regenerate into the drive.

This means that even if an RCD feeding the drive trips, this does not remove all sources of electrical charge, and this may induce a false sense of safety in the user.

For this reason it is best to avoid RCDs where possible, and to rely on conventional protective bonding to ensure electrical safety.

Section 5 EMC ISSUES

5.1 THE EMC DIRECTIVE

The EMC Directive is administered in the same way as the Machinery Directive, and the Low Voltage Directive.

The EMC directive (89/336) requires that electrical/electronic equipment must work correctly when installed and operated in its intended electromagnetic environment. In addition it must not cause interference to other equipment or services. In essence, no piece of equipment may emit undue electromagnetic emissions or be unduly susceptible to external emissions.

Electromagnetic disturbances can arise from both conducted emissions and radiated emissions. **ElectroMagnetic Compatibility (EMC)** is a balance of the emissions from a

particular apparatus and the immunity of that apparatus from disturbances caused due to emissions from external sources and these requirements are enshrined as the essential protection requirements of the EMC.

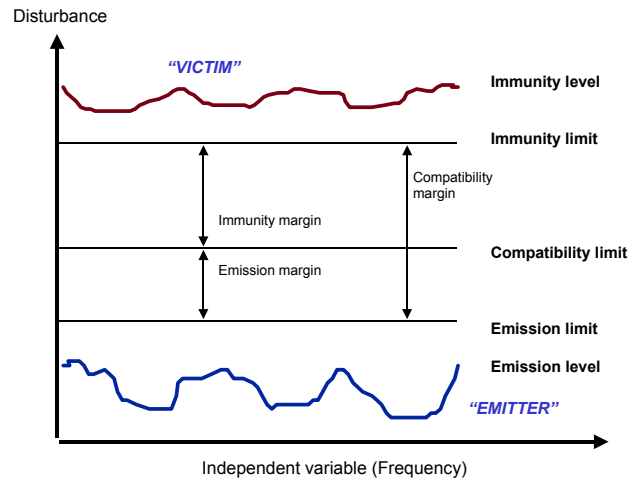


Figure 12 - Aspects of EMC

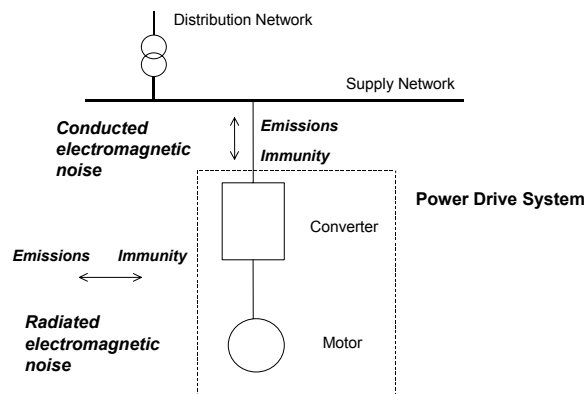


Figure 13 EMC aspects of a power drive system

Drive manufacturers take extensive design precautions, which both minimise the emissions of electromagnetic disturbances and maximise the immunity to externally generated noise. However, irrespective of the rigorous design parameters implemented by manufacturers, the integrity of the overall system is fundamentally dependent on the installation techniques adopted.

Immunity to external disturbances is achieved by the basic design in combination with high integrity high frequency earthing systems. Protection from radiated emissions is dependent on containment within the system using an effective shielding system – particularly in VSD output cables that carry the pwm waveform. Over and above the filtration included in standard drives, additional mitigation of the conducted noise may be specified using optional filtering.

5.2 STANDARDS

Firstly, we consider “Generic” standards, which apply generally, except where specific product standards apply.

Generic standards which may be relevant include:-

- EN 61000-6 parts 1 & 2 (Immunity)
- EN 61000-6 parts 3 & 4 (Emissions)

For variable speed drives however, there is a product specific standard: EN61800-3 “Adjustable speed electrical power drive systems - Part 3: EMC requirements and specific test methods”. The standard contains conformity assessment requirements as well as recommended engineering practice. The requirements of the product specific standard supersede the requirements of the generic standards, unless the PDS is built into another product e.g. a lift for which there is another specific product standard.

EN 61800-3 covers two environments:

- **“First environment”** where the point of coupling with domestic users of the public electricity supply is at low voltage, or
- **“Second environment”** where the point of coupling is above 1000V a.c.

The standard also covers two modes of commercial distribution:

- **“Restricted distribution”** - sold to professional users only, or
- **“Unrestricted distribution”** - available to the general public

This allows for differing levels of communication between supplier and vendor, for standard and purpose built equipment. The definition of actual use will predominantly affect the requirements for both emissions and immunity.

Whilst no explicit demands exist, the overriding requirement is always to meet the essential protection requirements of the EMC directive. Practically, the specific requirements of a particular VSD installation may be established by considering the following points

- 1) *The intended environment for the equipment use*
- 2) *The route to market (i.e. restricted or unrestricted)*
- 3) *The risk of interference with low immunity equipment*
- 4) *The consequences of interference*

The practical implementation of these issues need to be resolved for each case, but the examples in Section 5.9 give guidance.

5.3 MOTORS

As previously stated motors are essentially benign, unless fed from a converter. In this case the motor becomes a part of the “Faraday Cage” which restricts radiated emissions. For this purpose, all separate parts of the motor frame must be adequately bonded and joints may need to be filled with conductive gaskets.

5.4 CONVERTERS

The converter is the main source of electromagnetic noise; potential radiated emissions must be contained within a “Faraday Cage” which may well include the motor and cables.

Conducted emissions are generally controlled by a filter (see Section 5.7).

5.5 TRANSFORMERS

Transformers are again benign components, which will not generate disturbances, however, if a new transformer is being specified, consideration should always be given to fitting an earthed screen between primary and secondary windings, which has a substantial filtering effect on high frequency conducted emissions.

5.6 CABLES

Correct cable selection is essential to achieve good EMC performance, especially to attenuate radiated emissions. If screened cables are not practical in a particular installation, the use of a sinusoidal output filter should be considered.

5.7 FILTERS

Conducted emissions filters are sometimes referred to as RFI filters or EMC filters. These are always fitted to the supply side of a converter. Many manufacturers will offer integrated or “footprint” designs, which minimise the installation dimensions.

Typically, filters are available to meet so called “Class A” and “Class B” limits. The level of conducted emissions fed back into the supply will be dependent on the (shielded) motor cable lengths and the limits “A” and “B”⁷ will be met only with limited cable lengths as specified by the suppliers. Suppliers have an obligation to identify suitable filters.

Basic emission test methods and levels are given in CISPR standards CISPR 11 and CISPR 22. The generic and PDS standards are based on these, but use different terminology for their specific purposes. The following table shows how they correspond.

⁷ Emission levels defined in CISPR 11

CISPR 22 class	CISPR 11 class	Generic emissions standards - environment	EN 61800-3 – environment - distribution mode
B	B	EN 61000-6-3 - Residential, commercial & light industrial	First environment - unrestricted
A	A group 1	EN 61000-6-4 - Industrial	First environment - restricted
-	A group 2	-	Second environment - unrestricted
-	-	-	Second environment - restricted

Table 1 Comparison of class and environment terminology in the EMC emissions standards

5.8 EARTH CONDUCTORS

In general, good EMC requires low impedance bonding between the different parts of the PDS. It is a requirement for safety that the minimum potential equalising conductor should be at least 50% of the current carrying capacity of the main phase conductor.

Multi stranded cables and braids provide better high frequency conductance.

5.9 PRACTICAL EXAMPLES OF EMC AND PRODUCT SELECTION

- An 0.55kW PDS used for automatic garage door opening

As this unit is intended to be used in a domestic environment connected to the public low voltage supply, it is clearly in the “first environment”.

In this case, this is also potentially in unrestricted distribution and therefore a “class B” type filter to meet the generic “residential” emission requirements would be included.

- A 1000kW PDS in a Steel Rolling Mill

A steel mill would invariably take its incoming power supply at high voltage and have local HV/LV transformers to obtain the site low voltage supply. The mill is therefore in the “second environment”, and the PDS would be supplied through restricted distribution. In this case, there are likely to be many other electrical & electronic loads and the equipment used would be intended for such environments (e.g. would have a high immunity). By considering the effects of the new equipment on the installation, a site-specific EMC plan would be constructed. Typically, this would conclude that no additional conducted EMC filtering is required and standard “unfiltered” drives may be selected.

- One booster pump drive in a water pipeline

A small pumping station may well be supplied from an HV/LV transformer which also feeds residential properties in the vicinity. This is therefore a “first environment”, supplied in restricted distribution. Considering these criteria, a VSD with filtering at least to class A would be recommended.

- Sixty Drives in a Supermarket For HVAC Duties.

Typically, the building would contain integral HV/LV transformers and may therefore be considered in the “second environment”, and in restricted distribution. However, the EMC plan may determine that within the building, there will be numerous items of electronic apparatus such as computers, Point of Sale equipment, environmental monitoring instruments etc. connected to the same LV supply. Considering the criteria, VSDs with filtering at least to class A would typically be recommended.

- Sixty Drives To Be Installed In a Hospital For HVAC Duties

Again, the building would normally be supplied via a local HV/LV transformer and might therefore be considered as a “second environment”, and in restricted distribution. However, there are obviously considerable quantities of potentially susceptible medical apparatus – with the severe consequences of failure.

Therefore a cautious approach should be implemented and VSDs with “class B” filtering would be recommended.

As some supplies in a hospital environment will be “IT”, care must be taken to ensure that the filtered drives are connected to a “TN” network. The majority of RF Filters do not function in IT networks.

Notes.

In each of the above examples, the correct installation techniques remain a fundamental pre-requisite.

For each installation, the specific local conditions should be assessed within the EMC plan.

In each case, the essential protection requirements of the EMC directive must be observed.

5.10 HARMONICS

Harmonic emissions are an aspect of EMC which are largely governed by local regulations. They are a site-specific requirement and, within the UK, are governed by the Electricity Association Engineering recommendation G5/4. No PDS can in itself meet G5/4, only the entire clients site at the point of common coupling can comply. For information on compliance, the GAMBICA Guide to G5/4 is available.

5.11 RESPONSIBILITIES

All parties in the chain of supply have responsibilities to meet the requirements of the EMC directive (and all other relevant directives).

5.11.1 MANUFACTURER

The manufacturer has a duty to design products in a way that enables the EMC requirements to be met with realistic installation procedures. The manufacturer must also give detailed instructions in the installation guidelines – which are a pre-requisite to meeting the EMC directive.

Further, the manufacturer should be able to recommend the appropriate conducted EMC filters to be able to meet EMC mitigation levels -> normally specified as “class A” or “class B” filters.

The manufacturer should also be able to provide estimates of harmonic currents.

5.11.2 PANEL BUILDER

The panel builder / MCC manufacturer must follow the manufacturer’s installation instructions to achieve a reliable and “compliant” system. The installation instructions will cover basic safety issues, EMC mitigation measures and general installation issues such as cooling etc.

5.11.3 SYSTEM INTEGRATOR/INSTALLER

The system integrator or installer should ensure that the correct products have been selected with appropriate measures for the intended electromagnetic environment and installed in a rigorous way. Aspects such as “earthing”, grounding and shielding require particular attention.

5.11.4 USER

The equipment selection is dependent on the final use – e.g. domestic, industrial (see examples above). For industrial use, the end customer should specify the necessary site conditions and should also oversee the installer to ensure that the complete system is appropriate for the intended use.

For any given (industrial) application, the potential implications of installing the new equipment should be considered. Analysing the four criteria given in Section 5.2 above will form the basis of the site “EMC plan” and will therefore determine the required level of EMC mitigation. Ideally, the assessment will be done in consideration of the basic data supplied from the manufacturer. Guidance is given within EN 61800-3.

The user will also have a responsibility to ensure that the equipment is maintained in accordance with the manufacturer’s instructions.

Section 6 PROBLEM INSTALLATIONS

Very often problem installations are not immediately apparent, as can be seen from the following examples

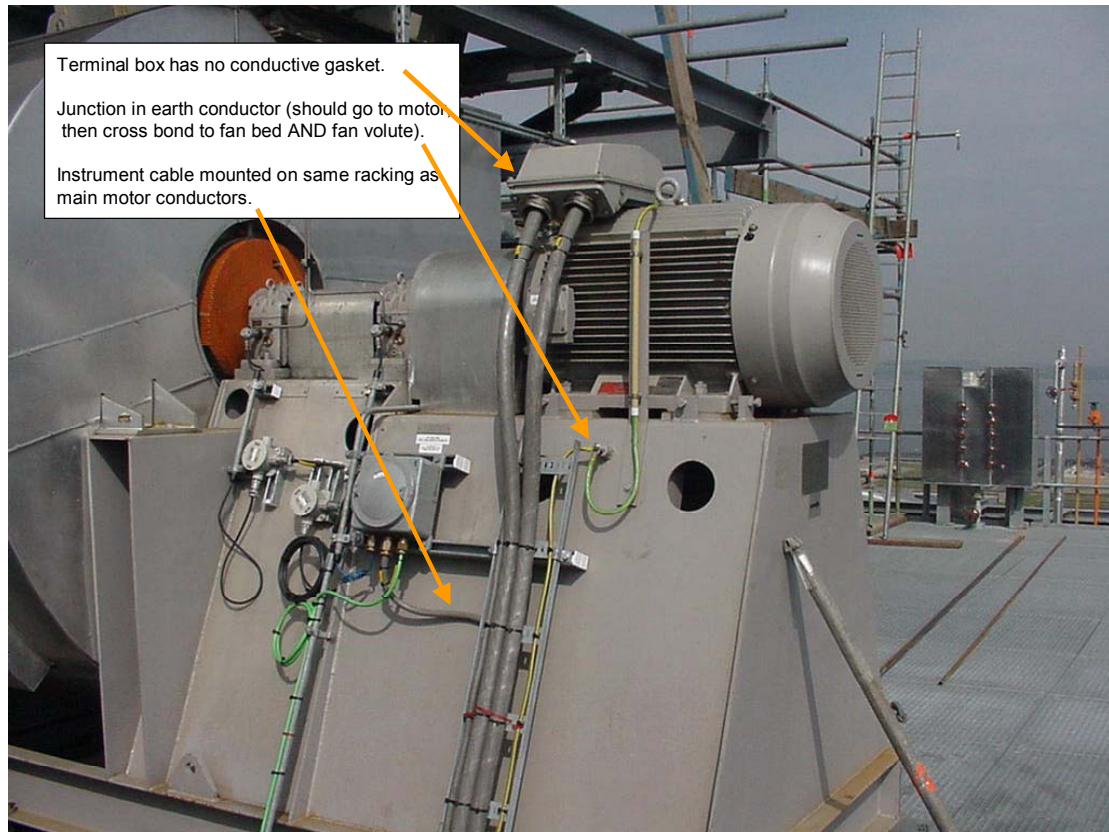


Figure 14 – Problem Example No 1

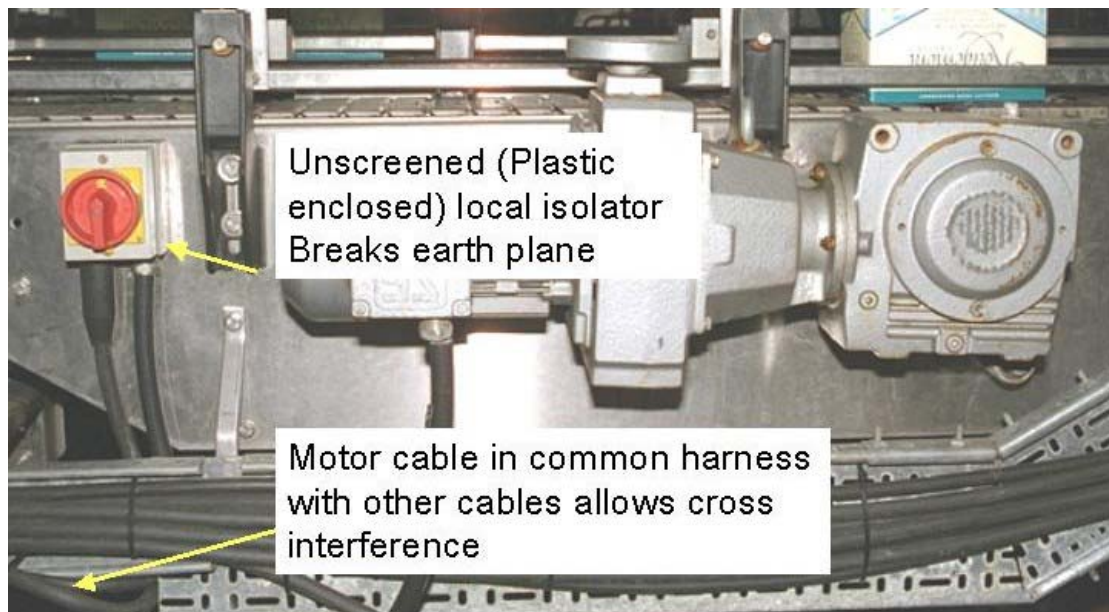


Figure 15 - Problem Example No 2

Section 7 GLOSSARY OF TERMS

TERM OR ABBREVIATION	DESCRIPTION	SECTION
a.c.	Alternating current	
Armour	A sheath fitted around a cable to provide mechanical protection	2.4 et seq
ATEX	“Atmosphères Explosible” – European Directive using French acronym, covering the essential health and safety requirements for products used in potentially explosive atmospheres	Specifically excluded from this Guide
BDM	Basic Drive Module	1.1
BSI	British Standards Institution – responsible for the preparation of UK National Standards, prefixed BS *** and publication of harmonised standards, prefixed BS-EN ***	
CE Mark	Indication of compliance with EU Directives	2.1
CENELEC	European Committee for the Electrotechnical Standardisation – responsible for the preparation of harmonised (EN) standards	
CISPR	Comité International Spécial des Perturbations Radioélectriques. (English – International Special Committee on Radio Interference) Prefix for standards prepared by this organisation (Published by the IEC q.v.)	5.7
COSHH	Control of Substances Hazardous to Health – UK Statutory requirements. See SI 2002/2677, etc	2.3.4.1
d.c.	Direct Current	
Earth/Earthing	Ground/Grounding - Terms used interchangeably	4
ELCB	Earth Leakage Circuit Breaker	4.2.3
EMC	Electromagnetic compatibility	5
EMI	Electromagnetic Interference	5
EN	EuroNorm – Standard issued by CENELEC, normally prefixed by the national issuing body e.g. BS EN	
Ethernet	Standards for serial communications interfaces	
EU	European Union	2
Faraday Cage	Term for an electromagnetic screen	
G5/4	UK requirements for harmonics	5.10
IEC	International Electrotechnical Commission – International Standardisation Body Prefix for standards prepared by this organisation	

IEEE 519	American Standard - IEEE Recommended Practices and Requirements for Harmonic Control in Electrical Power Systems	3.6
I/O	Input/Output (connections)	3.15
IT	Ungrounded network	4.1.2
MCB	Miniature circuit breaker	3.8
MCC	Motor Control Centre	5.9
MCCB	Moulded case circuit breaker	3.8
“noise”	Electromagnetic Interference	5
PDS	Power Drive System	1.1
PE	Protective Earth	4
PWM	Pulse Width Modulated	1.3
RCD	Residual current detecting device – form of earth leakage protection	4.2.3
RS 232/485	Standards for serial communications interfaces	3.15.3
r.m.s.	Root mean square	
RTD	Resistance temperature detector	
Screen	An electromagnetic barrier	
SI	Statutory Instrument	2.1
TN, TN-C, TN-S	Earthed neutral networks	4.1.1
UL	Underwriters Laboratories – American inspection and certification organisation.	
12-pulse	Technique to reduce harmonics	See GAMBICA Guide to G5/4

Section 8 KEY EUROPEAN DIRECTIVES AND PRINCIPAL ASSOCIATED STANDARDS

Electrical Safety:

Directive 73/23/EEC Electrical equipment designed for use within certain voltage limits (Low Voltage Directive)

93/68/EEC Amendment of 73/23/EEC.

EN 60034 – Various parts – Standards relating to Electric Motors.

EN 60204-1:1997 + corrigendum Sept 1998, Safety of Machinery – Electrical equipment of machines Part 1:General requirements

Machinery Safety:

Directive 98/37/EC (Machinery Directive)

EN 292-1:1991 Safety of Machinery – Basic concepts, general principles for design Part 1:Basic Terminology, methodology

EN 292-2:1991 + A1:1995 Safety of Machinery – Basic concepts, general principals for design Part 2:Technical Principles and specifications

EN 418:1992 Safety of Machinery – Emergency stop requirements, functional aspects. Principles for design

EN 954-1:1996 Safety of Machinery – Safety-related parts of control systems Part 1:General principles for design

EN 1037:1996 Safety of Machinery – Prevention of unexpected start-up

EN 1050:1996 Safety of Machinery – Principles of risk assessment.

EN 60204-1:1997 + corrigendum Sept 1998,Safety of Machinery – Electrical equipment of machines Part 1:General requirements

Electromagnetic Compatibility:

89/336/EEC Electromagnetic Compatibility Directive

92/31/EEC Amendment to directive 89/336/EEC

93/68/EEC Amendment to directive 89/336/EEC

EN 61000-6-x Generic EMC standards

EN 61800-3:1996 + Amendment A11 Adjustable speed electrical power drive systems Part 3:EMC product standard including specific test methods

Section 9 FREQUENTLY ASKED QUESTIONS

Q - If I have several motors to run at the same speed, how do I select a frequency converter?

A - In multi-motor configuration where a number of motors are fed from a single inverter the sum of the motor currents must be less than the rated current of the inverter. If the motors are started simultaneously, the total acceleration current must be less than the overload current of the inverter.

When motors are started sequentially at any frequency, as the direct on line (DOL) starting current (typically 5 to 8 times full load current) flows into the motor, this peak current must be accounted for and the maximum current must not exceed the overload current rating of the inverter.

The sum of the rated motor currents after completion of the start must be less than the rated inverter output current.

Each motor will require individual protection, as the integral protection afforded by the converter will only see the group of motors. Great care must be taken in selecting suitable protection, as many protection devices do not function satisfactorily in an inverter output.

When considering the maximum cable lengths permitted the sum of all the cables fitted in the inverter must be considered.

Q - How frequently should the mains supply of a Frequency Converter drive be switched on / off ?

A - This will depend on the individual manufacture. However typically a gap of at least three minutes will be required, otherwise the internal inrush current limitation could be overloaded.

Normally a drive should be started and stopped by the control electronics. Frequent opening for example of safety interlocks may require output switching.

Q - How should a power supply cable shield be connected?

A - Supply cable shields must always be grounded at the supply source end; usually the converter end will be grounded at the converter. Cables should always be properly terminated using the appropriate glands to give 360° shield termination. However, with single cores the shield must always be left unconnected and isolated at the converter end to prevent circulating currents.

Q - For most motors the thermal loadability drops as the speed reduces; how do we protect the motor?

A - Basically a conventional motor thermal overcurrent relay would allow a motor to draw too high a current at low speed, and is therefore unreliable.

An embedded thermal device is always one method of obtaining protection; thermostats, PTC thermistors or RTD devices may all be used with an appropriate external relay. Some drives will also integrate thermistor monitoring.

As the inverter controls the speed and monitors the motor current, it can also provide motor protection, based on the load and speed, and compensate for reduced loadability at reduced speed.

Some more sophisticated drives offer both over and under load protection, which allows monitoring of coupling failure or possibly low flow.

Q - What limits a motor maximum speed?

A - A motor is not limited to its mains supply frequency synchronous speed; it can be both reduced and increased. Beyond base speed the torque available will drop as the inverter cannot increase its output voltage and the motor becomes progressively under fluxed. This is known as field weakening

There is a specific maximum output speed for any motor, based on two factors:-

- The mechanical maximum speed, these are normally limited by the bearings and peripheral velocities, typical values for standard TEFV motors with grease lubricated ball bearings are.
- The electrical maximum speed, which is due to the reduction in flux causing the available maximum torque to reduce as the square of the increase in frequency.

For larger 2-pole motors it is common to design with a “flexible shaft” design, which also precludes running at critical speeds below the nominal speed.

The advice of the manufacturer should be sought especially before: -

- running any motor above its base speed,
- running any 2 pole unit constructed motor at variable speed
- running any motors which include self lubricated sleeve bearings

Q - What is the likely effect on reliability of including a drive within my system?

A - Frequency converters have been available in the market place for over 25 years, and have improved in reliability over this time.

Subject to satisfactory installation and routine maintenance, including removal of dust, cleaning cooling surfaces, and regular replacement of limited lifetime parts, such as cooling fans, together with regular pump and motor bearing lubrication and maintenance, a modern drive system should have a long and satisfactory life.

Current manufacturers' experience shows the MTBF for the electronics increasing. Currently it is around 15 years to 30 years, depending on size and installation.

Q - I need to install an isolator local to the motor for safety purposes; what do I have to consider?

A - The isolator housing must continue the Faraday Cage screening the inverter output, and must be connected to the cable screen/armour.

Every junction in a cable will also be a substantial change in impedance which can cause voltage transients. As a rule of thumb, each junction can be considered to halve the maximum cable run approved by the drive manufacturer.

The editors invite further questions to be passed by e-mail to assoc@gambica.org.uk for inclusion in subsequent editions.

Section 10 REFERENCES AND ACKNOWLEDGEMENTS

- [1] IEC 60034-17: 1998 Cage induction motors when fed from converters - Application guide
- [2] GAMBICA/REMA Technical Report No 1 – Motor Insulation Voltage Stresses under PWM Inverter Operation
- [3] GAMBICA/REMA Technical Report No 2 – Motor Shaft Voltages and Bearing Currents under PWM Inverter Operation
- [4] GAMBICA Technical Guide – General Purpose Enclosures.
- [5] GAMBICA Technical Guide – Managing Harmonics : A guide to EA Engineering Recommendation G5/4
- [6] NEMA ‘Application Guide for AC Adjustable Speed Drive Systems’

This guide has been prepared by GAMBICA's Variable Speed Drives Group + REMA.



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GAMBICA is the Association for Instrumentation, Control, Automation & Laboratory Technology and has a group specifically for suppliers of Variable Speed Drives.

REMA is the Rotating Electrical Machines Association representing manufacturers of rotating electrical machines, other than turbine machines, traction motors or machines for the use in aircraft.

The greatest care has been taken to ensure the accuracy of the information contained in this guide, but no liability can be accepted by GAMBICA, REMA or their members, for errors of any kind.

Always refer to your Drive and Motor Suppliers if in doubt about correct matching.